



Summary

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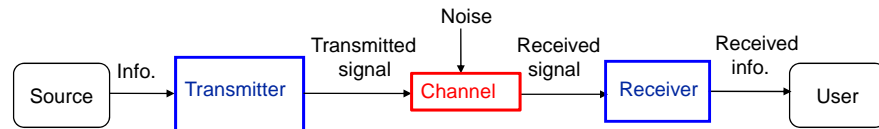
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What matter we covered

- Antennas in a system
 - Friis' formula (transceiver-channel-receiver)
- Transceiver side : EIPR
- Channel : path loss
- Receiver side : G/T (includes antenna and receiver noise)

General wireless link



Received power:

Attenuation due to propagation

$$P_R = P_T G_T \frac{1}{\left(\frac{4\pi D}{\lambda}\right)^2} G_R = P_T G_T \frac{1}{\alpha_0} G_R$$

In decibel:

$$\begin{aligned}
 P_R \text{ dBW} &= P_T \text{ dBW} + G_T \text{ dB} - \alpha_0 \text{ dB} + G_R \text{ dB} \\
 &= \text{EIRP} \text{ dBW} - \alpha_0 \text{ dB} + G_R \text{ dB}
 \end{aligned}$$



EIRP (Equivalent Isotropic Radiated Power)

- ★ Is the product (the sum in logarithmic units) of the transmitted power and the gain of the transmit antenna
- ★ It is directly derived from the definition of the antenna gain
- ★ It represents the power applied at the input of an isotropic radiator in order to obtain the same power density as that of the real case



Path loss

- Power of wireless transmission reduces with square of distance (due to surface area increase of sphere)
- Reduction also depends on wavelength
 - Long wave length (low frequency) has less loss
 - Short wave length (high frequency) has more loss

$$P_L = \left(\frac{4\pi D}{\lambda} \right)^2$$

Path loss exponent



Path loss

Different path loss exponents are used in different environments:

Free space	2
Urban area cellular	2.7 to 3.5
Shadowed urban cell	3 to 5
In building Line Of Sight	1.6 to 1.8
Obstructed in building	4 to 6
Obstructed in factories	2 to 3



SIGNAL TO NOISE RATIO

- ★ We often use, in order to evaluate power level relative to noise, the ratio:

$$\gamma = \frac{P_R}{N_0}$$

where: P_R = Received power

N_0 = Noise power spectral density

- ★ Such a ratio is used for any modulation scheme, analog or digital



- ★ The ratio γ has the dimension of frequency; all together, for this expression one specifies a logarithmic unit (dBHz)

- ★ The spectral density level N_0 equals:

$$N_0 = K T_{op}$$

where K = Boltzmann's constant $= 1.38 \cdot 10^{-23}$

T_{op} = Effective temperature of the receiver $(= T_A + T_R)$



- ★ Hence:

$$\gamma = \frac{P_R}{N_0} = \frac{P_R}{K T_{op}}$$

And in logarithmic units:

$$\gamma|_{\text{dBHz}} = P_R|_{\text{dBW}} - 10 \cdot \log_{10} K - 10 \cdot \log_{10} T_{op} + 228.6$$

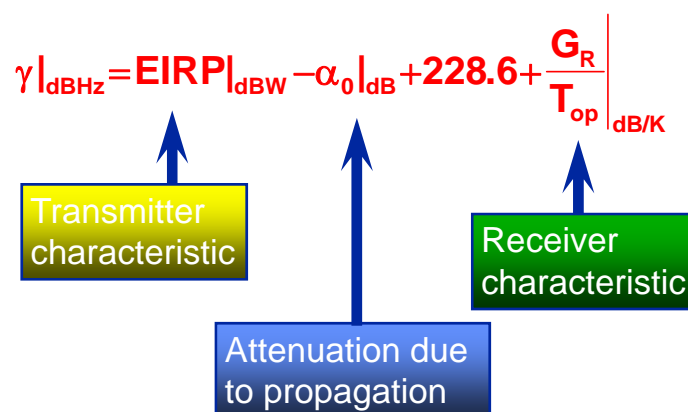
★ Substituting the expression for $P_R|_{\text{dBW}}$

$$\gamma|_{\text{dBHz}} = \text{EIRP}|_{\text{dBW}} - \alpha_0|_{\text{dB}} + 228.6 + G_R|_{\text{dB}} - 10 \cdot \log_{10} T_{\text{op}}$$

$$10 \cdot \log_{10} \frac{G_R}{T_{\text{op}}} = \frac{G_R}{T_{\text{op}}} \Big|_{\text{dB/K}}$$

From which:

$$\gamma|_{\text{dBHz}} = \text{EIRP}|_{\text{dBW}} - \alpha_0|_{\text{dB}} + 228.6 + \frac{G_R}{T_{\text{op}}} \Big|_{\text{dB/K}}$$





Antenna parameters

- Gain: G
- Directivity D
- efficiency: η
- effective aperture: A_e
- radiation pattern: $E(\theta, \phi)$, $p(\theta, \phi)$
- antenna input impedance: Z_a
- antenna input reflection coefficient: s_{11}
- polarization: linear, circular or elliptic

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Antenna pattern

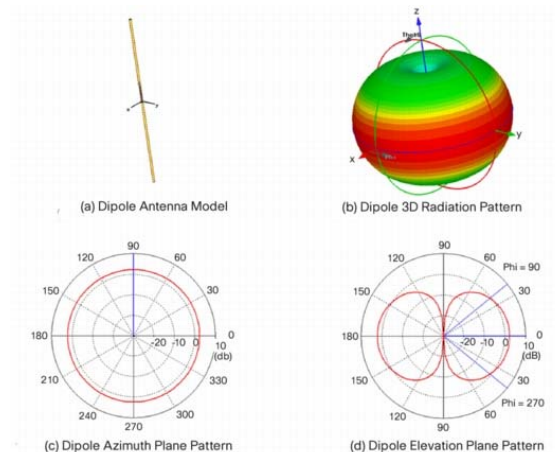


Image from: http://www.cisco.com/c/en/us/products/collateral/wireless/aironet-antennas-accessories/prod_white_paper0900aecd806a1a3e.html

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Antenna gain

An imaginary radiation pattern assuming all the energy is transmitted in the same power in all directions. (This is a reference point for Antenna Gain Calculation)

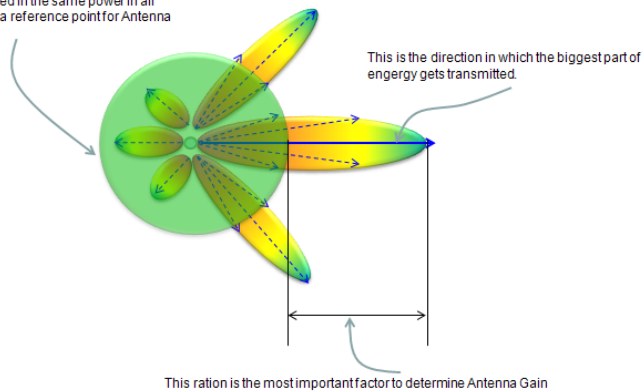


Image from : http://www.sharetechnote.com/html/Handbook_LTE_AntennaPerformance.html

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Antenna parameters

$$G(\theta, \varphi) = \eta D(\theta, \varphi)$$

$$G(\theta, \varphi) = \frac{4\pi}{\lambda^2} A_e(\theta, \varphi)$$

$$S_{11} = \frac{Z_a - Z_{gen}}{Z_a + Z_{gen}}$$

Z_{gen} is the impedance of the generator
(transmitter) or the load (receiver)

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Friis formula (ideal)

In free space

$$P_r = P_{tr} g_r g_{tr} \left(\frac{\lambda}{4\pi R} \right)^2$$

in general

$$P_r = P_{tr} g_r g_{tr} \left(\frac{\lambda}{4\pi R} \right)^\alpha$$



Friis formula (real)

In free space

$$P_r = P_{tr} g_r g_{tr} (1 - \rho_r^2)(1 - \rho_{tr}^2) \left(\frac{\lambda}{4\pi R} \right)^2 |\mathbf{pol}_{tr} \cdot \mathbf{pol}_r^*|^2$$

in general

$$P_r = P_{tr} g_r g_{tr} (1 - \rho_r^2)(1 - \rho_{tr}^2) \left(\frac{\lambda}{4\pi R} \right)^\alpha |\mathbf{pol}_{tr} \cdot \mathbf{pol}_r^*|^2$$

depolarization factor

$$\chi_{pol} = |\mathbf{pol}_{tr} \cdot \mathbf{pol}_r^*|^2$$

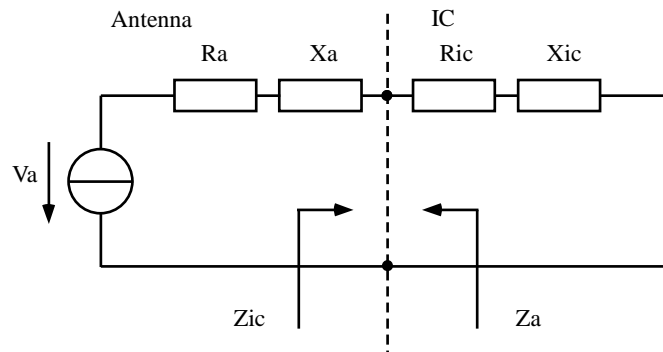
ρ_r : reflection coefficient of receiving antenna

ρ_{tr} : reflection coefficient of transmitting antenna

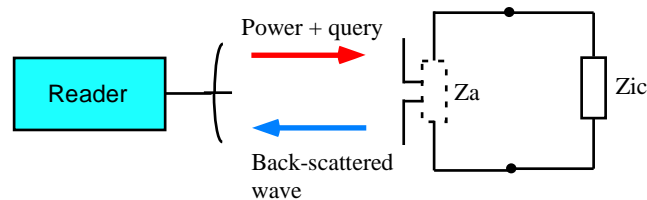
\mathbf{pol}_r : polarisation vector of receiving antenna

\mathbf{pol}_{tr} : polarisation vector of transmitting antenna

Antennas in RFID scenarii



power scavenging and backscattering



$$P_{load} = S_i(r, \theta, \varphi) A_{e, \max} \tau \chi_{pol} = S_i(r, \theta, \varphi) G_r(\theta, \varphi) \frac{\lambda^2}{4\pi} (1 - |\Gamma^*|^2) \chi_{pol}$$

$$S_{scat} = \frac{P_{re-rad} G_r(\theta, \varphi)}{4\pi r^2} = S_{t, inc}(\theta_{inc}, \varphi_{inc}) \frac{\lambda^2}{(4\pi r)^2} G_r(\theta_{inc}, \varphi_{inc}) |\Gamma^*|^2 G_r(\theta, \varphi) \chi_{pol}$$

- A good match is needed for the power transfer
- A large mismatch is required for the backscattering



figure of merit for RFIDs : max read range

$$r_{\max}(\theta, \varphi) = \frac{\lambda}{4\pi} \sqrt{\frac{G_{r, \text{real}}(\theta, \varphi) \chi_{\text{pol}} EIRP}{P_{ic, th}}}$$



Regulations and standards

- Each country has its own regulations
- Based on IEEE standards, FCC (US), ICNIRP (Europe)
- Some rules can be contradictory
- They change over time with the advance of science



Antennas for W-BAN

- They radiate at least partially into lossy media
- Most classic antenna characteristic definitions do not apply anymore
- Radiation into lossy medium is not well known



Antennas in/on biological tissues

- The medium will absorb a large amount of the power
- In order to optimize the design, we try to control the near field, use a magnetic type antenna and have an appropriate polarization (e.g. orthogonal to the wearer for a wearable antenna). We also try to use a ground plane.



Measurement of W-BAN antennas

- Implantable and wearable antennas are usually electrically small
- Their port might be ill defined leading to cable currents when connected to measurement devices and thus wrong results
- Some tricks can be used to overcome this
 - baluns, avoid contact of cable with lossy tissues, etc.
- But the only reliable measurements are system measurement with the antenna in their final setting.



Exam (antenna part)

- 1 exercise (same style as during class exercises)
- 3 multiple choice questions, with justification of the answer
- Do not forget your pocket calculator !!!